

Shape lb/ft	W21x					
	50		48 ^f		44	
	M_{nx}/Ω_b	$\phi_b M_{nx}$	M_{nx}/Ω_b	$\phi_b M_{nx}$	M_{nx}/Ω_b	$\phi_b M_{nx}$
Available Flexural Strength, kip-ft						
	ASD	LRFD	ASD	LRFD	ASD	LRFD
0	274	413	265	398	238	358
6	257	387	265	398	221	332
7	245	368	256	385	210	315
8	233	350	246	370	198	298
9	221	332	236	355	187	281
10	209	314	226	340	176	264
11	197	295	217	326	165	248
12	184	277	207	311	154	231
13	172	259	197	296	142	214
14	157	236	187	282	125	188

Design of Flexural Members

Figure 4 illustrates a magnified portion of a sample page from Table 6-2 with available flexural strengths listed on the right-hand side of the page.

Again, all W-sections are listed in the table, including those that may not be ordinarily used as beams but may be appropriate for certain situations.

Values of the available flexural strength listed in Table 6-2 meet the appropriate provisions of Chapter F of the *Steel Construction Manual* and account for compact/noncompact/slender-element section provisions of Section B4. Therefore, there is no need for width-to-thickness ratio checks of the selected W-section. Further, appropriate AISC equations have been used in developing the tabulated values with respect to the unbraced length of the beam relative to limiting unbraced lengths L_c and L_s . Thus, no additional check of the unbraced length is needed when using this table.

The procedures for design of a flexural member using Table 6-2 is similar to design for compression members described above. The designer enters the table with the unbraced length L_u of the beam and selects a W-section from the desired nominal depth with available flexural strength equal to or greater than the required strength. Note that flexural strengths are listed on the right half of the buttery formatted page. The left and right halves of the table are clearly labeled at the top to avoid confusion.

As an example, per Figure 4, an A992 W21×48 with an unbraced length of 10 ft has an available flexural strength of 226 kip-ft and 340 kip-ft based on the ASD and LRFD methods, respectively. Remember that a W21×48 of ASTM A992 is a non-compact beam section. However, Table 6-2 already accounts for this classification and there is no need to check the width-to-thickness ratio of the compression elements of this beam section. Also, there is no need to compare the unbraced length to λ_1 and λ_2 , though values of λ_1 and λ_2 are listed at the bottom of the page for convenience.

ASD Method:

$$P = 100 \text{ kips (compression)}, \quad () = \quad = 15 \text{ ft},$$
$$(M) = 150 \text{ kip-ft}, \quad (M) = 30 \text{ kip-ft}$$

Obtain the following from Table 6-2:

$$\text{For } () = 15 \text{ ft}, P / = 489 \text{ kips}$$

$$\text{For } = 15 \text{ ft}, M / = 254 \text{ kip-ft}$$

$$M / = 123 \text{ kip-ft}$$

B90 5.94 ause